

# GEOTECHNICAL INVESTIGATION

FOR

## NSW LAND & HOUSING CORPORATION

*38 – 42 Gerathy Street, Goulburn, New South Wales (BH2NM)*

*Report No: 24/0904*

*Project No: 32649/8602D-G*

April 2024

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DRAWING NO. 24/0904 – BOREHOLE AND PENETROMETER LOCATIONS

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## 1. INTRODUCTION

This report presents the results of a geotechnical investigation carried out by STS Geotechnics Pty Limited (STS) for a proposed new residential development to be constructed at 38 – 42 Gerathy Street, Goulburn, NSW. At the time of writing this report STS were not provided with architectural drawings for the project, however we understand the development will typically comprise the demolition of existing structures prior to construction of single or double storey residential buildings. The development will not include basement levels.

The purpose of the investigation was to determine:

- Site conditions and regional geology,
- Subsurface conditions,
- Site Classification to AS2870-2011 (soil reactivity),
- Foundation design parameters including foundation options, and
- Soil aggressiveness to buried steel and concrete in accordance with AS2870-2011 and AS2159-2009.

The investigation was undertaken at the request of NSW Land and Housing Corporation as outlined in STS's proposal referenced P24-126 dated March 13, 2024.

Our scope of work did not include a contamination assessment.

## 2. NATURE OF THE INVESTIGATION

### 2.1. Fieldwork

The fieldwork consisted of drilling five (5) boreholes numbered BH1 to BH5, inclusive, at the locations shown on Drawing No. 24/0904. The boreholes were drilled using a utility mounted Christie drilling rig, owned, and operated by STS. Soil strengths were determined by undertaking Dynamic Cone Penetrometer (DCP) tests adjacent to each borehole location.

Representative soil samples were collected for subsequent laboratory testing.

Drilling operations were undertaken by one of STS's senior technical officers who also logged the subsurface conditions encountered.

The subsurface conditions observed are recorded on the borehole logs given in Appendix A. An explanation of the terms used on the logs is also given in Appendix A. Notes relating to geotechnical reports are also attached.

## 2.2. Laboratory Testing

To assess the soils for their aggressiveness, three (3) selected representative soil samples were tested to determine the following:

- pH,
- Sulphate content ( $\text{SO}_4$ ),
- Chloride content (CL), and
- Electrical Conductivity (EC)

To assist with the site classification, three (3) selected representative soil samples were tested to determine the shrink/swell index.

Detailed test reports are given in Appendix B.

## 3. GEOLOGY AND SITE CONDITIONS

The Goulburn geological series sheet at a scale of 1:100,000 shows that the site is underlain by Cainozoic Age unconsolidated alluvial quartzose sand and polymictic gravel, silcrete and quartz – and iron cemented sandstone and conglomerate.

The site is roughly rectangular in shape with an area of approximately 2278 m<sup>2</sup>. At the time of the fieldwork, the site was occupied by single storey dwellings. Site vegetation comprises trees and grass. The ground surface falls about 0.5 metres to the east, across the site.

The site is bound by Gerathy Street to the east and residential dwellings in the adjoining properties.

## 4. SUBSURFACE CONDITIONS

When assessing the subsurface conditions across a site from a limited number of boreholes, there is the possibility that variations may occur between test locations. The data derived from the site investigation programme are extrapolated across the site to form a geological model and an engineering opinion is rendered about overall subsurface conditions and their likely behaviour regarding the proposed development. The actual condition at the site may differ from those inferred, since no subsurface exploration programme, no matter how comprehensive, can reveal all subsurface details and anomalies, particularly on a site such as this that has been previously developed.

The subsurface conditions consist of topsoil overlying natural silty clays. The topsoil is present from the surface to depths of 0.2 to 0.3 metres. Firm, becoming very stiff with depth, natural silty clays underlie the topsoil to the maximum depth of drilling, 3.0 metres.

No groundwater was observed during the site drilling.

## 5. GEOTECHNICAL DISCUSSION

### 5.1. Site Classification to AS2870-2011

The classification has been prepared in accordance with the guidelines set out in the “Residential Slabs and Footings” Code, AS2870 – 2011.

To assist with determining the site classification, three (3) representative samples were retrieved from site for shrink swell testing. The test report is attached and summarised in Table 5.1.

Table 5.1 – Shrink Swell Test Summary

Location	Depth (m)	Material Description	Shrink/Swell Index (% per $\Delta pF$ )
BH1	0.8 – 1.0	Yellow brown silty clay, with gravel	2.7
BH3	1.2 – 1.4	Yellow brown silty clay, with sand	2.2
BH5	1.0 – 1.2	Yellow brown orange, with sand	0.9

Because there are trees and existing dwellings present, abnormal moisture conditions (AMC) prevail at the site. (Refer to Section 1.3.3 of AS2870-2011).

Because of the AMC, the site may be classified as a *Problem Site (P)*. However, provided the recommendations given below are adopted, the site may be reclassified as *Highly Reactive (H1)*.

Foundation design and construction consistent with this classification shall be adopted as specified in the above referenced standard and in accordance with the design parameters provided below.

### 5.2. Foundation Design

Because of the low bearing strength, we do not recommend founding footings within the firm soils.

Pad and/or strip footings founded in the stiff natural silty clays may be proportioned using an allowable bearing pressure of 100 kPa. The minimum depth of founding must comply with the requirements of AS2870-2011. To overcome the presence of trees, the foundations should be designed in accordance with the procedures given in Appendices H and CH of AS2870-2011.

Piers founded in very stiff natural silty clays may be proportioned using an allowable bearing pressure of 300 kPa, provided the depth to diameter ratio exceeds a value of 4. An adhesion value of 20 kPa may be adopted.

To ensure the bearing values given can be achieved, care should be taken to ensure that the base of excavations is free of all loose material prior to concreting. It is recommended that all shallow footing excavations be protected with a layer of blinding concrete as soon as possible, preferably

immediately after excavating, cleaning, inspection, and approval. Pier excavations should not be left open overnight.

The site is considered suitable for slab on ground construction provided the slab is proportioned for an allowable bearing pressure of 50 kPa when founding within firm materials.

During foundation construction, should the subsurface conditions vary to those inferred in this report, a suitably experienced geotechnical engineer should review the design and recommendations given above to determine if any alterations are required.

### 5.3. Soil Aggressiveness

The aggressiveness or erosion potential of an environment in building materials, particularly concrete and steel is dependent on the levels of soil pH and the types of salts present, generally sulphates and chlorides. To determine the degree of aggressiveness, the test values obtained are compared to Tables 6.4.2 (C) and 6.5.2 (C) in AS2159 – 2009 Piling – Design and Installation. The test results are summarised in Table 5.2.

Table 5.2– Soil Aggressiveness Summary

Sample No.	Location	Depth (m)	pH	Sulfate (mg/kg)	Chloride (mg/kg)	Electrical Conductivity (dS/m)	
						EC <sub>1:5</sub>	EC <sub>e</sub>
S1	BH1	0.2	7.7	<10	20	0.070	0.6
S2	BH3	0.2	7.9	<10	<50	0.038	0.4
S3	BH5	0.2	8.0	<10	<50	0.046	0.4

The soils on the site are low permeability and above groundwater. Therefore, soil conditions B are considered appropriate (AS2159).

A review of the durability aspects indicates that:

- pH : minimum value of 7.7
- SO<sub>4</sub> : maximum value of <10 mg/kg (ppm) < 5000 ppm
- Cl : maximum value of <50 mg/kg (ppm) < 5000 ppm
- EC<sub>e</sub> : maximum value of 0.6 dS/m

In accordance with AS2159-2009, the exposure classification for the onsite soils are non-aggressive to both steel and concrete. In accordance with AS2870-2011 the soils are classified as A1.

Reference to DLWC (2002) "Site Investigations for Urban Salinity" indicates that  $EC_e$  values of 0.4 to 0.6 dS/m are consistent with the presence of non-saline soils.

## 6. FINAL COMMENTS

During construction, should the subsurface conditions vary from those inferred above, we would be contacted to determine if any changes should be made to our recommendations. The exposed bearing surfaces for footings should be inspected by a geotechnical engineer to ensure the allowable pressure given has been achieved.

The above classification has been made assuming that all footings will bear in either natural ground or in controlled filling. Prior to the placement of any filling the existing surface should be stripped of all vegetation and topsoil.

If excavations for rainwater or detention tanks are to be made within 6 metres of the building foundations, advice should be sought regarding their effect on the foundations.

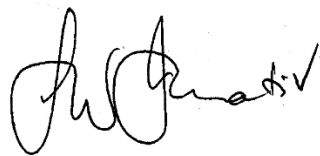
Placing absorption trenches on the high side of the property may create abnormal moisture conditions for the foundations (Refer to Section 1.3.3 of AS2870-2011). This could have a negative effect on the foundation performance and more than likely alter the site classification provided above.

This report has been prepared assuming that no trees other than those noted will be present on the site. If future tree planting is planned, eg. there is a landscaping plan, their effect on the foundation performance must be considered.

This report has been prepared assuming the site development will be limited to one or two storey residential buildings. The information and interpretation may not be relevant if the design proposal changes (e.g. to a five-storey building involving major cuts during the site preparation). If changes occur, we would be pleased to review the report and advise on the adequacy of the investigation.



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## Borehole and Penetrometer Locations

Client:	HOMES NSW	Project No.	32649/8602D-G	Date:	April 2024
Site Address:	38-42 Gerathy Street, Goulburn	Drawing No.	24/0904	Scale:	Unknown
Work:	Geotechnical Investigation	Revision No.	0		



## INTRODUCTION

These notes have been provided to outline the methodology and limitations inherent in geotechnical reporting. The issues discussed are not relevant to all reports and further advice should be sought if there are any queries regarding any advice or report. When copies of reports are made, they should be reproduced in full.

## GEOTECHNICAL REPORTS

Geotechnical reports are prepared by qualified personnel on the information supplied or obtained and are based on current engineering standards of interpretation and analysis.

Information may be gained from limited subsurface testing, surface observations, previous work and is supplemented by knowledge of the local geology and experience of the range of properties that may be exhibited by the materials present. For this reason, geotechnical reports should be regarded as interpretative rather than factual documents, limited to some extent by the scope of information on which they rely.

Where the report has been prepared for a specific purpose (eg. design of a three-storey building), the information and interpretation may not be appropriate if the design is changed (eg. a twenty storey building). In such cases, the report and the sufficiency of the existing work should be reviewed by STS Geotechnics Pty Limited in the light of the new proposal.

Every care is taken with the report content, however, it is not always possible to anticipate or assume responsibility for the following conditions:

- Unexpected variations in ground conditions. The potential for this depends on the amount of investigative work undertaken.
- Changes in policy or interpretation by statutory authorities.
- The actions of contractors responding to commercial pressures.

If these occur, STS Geotechnics Pty Limited would be pleased to resolve the matter through further investigation, analysis or advice.

## UNFORSEEN CONDITIONS

Should conditions encountered on site differ markedly from those anticipated from the information contained in the report, STS Geotechnics Pty Limited should be notified immediately. Early identification of site anomalies generally results in any problems being more readily resolved and allows re-interpretation and assessment of the implications for future work.

## SUBSURFACE CONDITIONS

Logs of a borehole, recovered core, test pit, excavated face or cone penetration test are an engineering and/or geological interpretation of the subsurface conditions. The reliability of the logged information depends on the drilling/testing method, sampling and/or observation spacings and the ground conditions. It is not always possible or economic to obtain continuous high quality data. It should also be recognised that the volume or material observed or tested is only a fraction of the total subsurface profile.

Interpretation of subsurface information and application to design and construction must take into consideration the spacing of the test locations, the frequency of observations and testing, and the possibility that geological boundaries may vary between observation points.

Groundwater observations and measurements outside of specially designed and constructed piezometers should be treated with care for the following reasons:

- In low permeability soils groundwater may not seep into an excavation or bore in the short time it is left open.
- A localised perched water table may not represent the true water table.
- Groundwater levels vary according to rainfall events or season.
- Some drilling and testing procedures mask or prevent groundwater inflow.

The installation of piezometers and long term monitoring of groundwater levels may be required to adequately identify groundwater conditions.

## SUPPLY OF GEOTECHNICAL INFORMATION OR TENDERING PURPOSES

It is recommended tenderers are provided with as much geological and geotechnical information that is available and that where there are uncertainties regarding the ground conditions, prospective tenders should be provided with comments discussing the range of likely conditions in addition to the investigation data.

## APPENDIX A – BOREHOLE LOGS AND EXPLANATION SHEETS

Client: Homes NSW Project: 38-42 Gerathy Street, Goulburn Location: Refer to Drawing No. 24/0904				Project: 32649/8602D-G Date : April 8, 2024 Logged: MB      Checked By: MT		BOREHOLE NO.: BH 1		
						Sheet 1 of 1		
W A T T A E B R L E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  Soil Name, grain size /plasticity, colour; secondary constituents (Inc. Description) , minor constituents including other remarks			S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
	S1 @ 0.6 m	0.0	TOPSOIL: SILTY CLAY: low plasticity, brown			CL	—	>PL
		0.1						
		0.2						
	U50	0.3	SILTY CLAY: low plasticity, grey brown			CL	FIRM	>PL
		0.4						
		0.5						
		0.6	SILTY CLAY: medium plasticity, yellow brown			CI	FIRM	>PL
		0.7					STIFF	
		0.8						
		0.9						
1.0								
		1.1						
		1.2						
		1.3						
		1.4						
		1.5						
		1.6						
		1.7						
		1.8						
		1.9						
		2.0						
		2.1						
		2.2						
		2.3						
		2.4						
		2.5						
		2.6						
		2.7						
		2.8						
		2.9						
		3.0	BOREHOLE DISCONTINUED AT 3.0 M				VERY STIFF	=PL
D - disturbed sample      U - undisturbed tube sample      B - bulk sample WT - level of water table or free water      N - Standard Penetration Test (SPT) S - jar sample					Contractor: STS Equipment: Christie Hole Diameter (mm): 100			
NOTES: See explanation sheets for meaning of all descriptive terms and symbols					Angle from Vertical (°): 0 Drill Bit: Spiral			



Client: Homes NSW				Project: 32649/8602D-G		BOREHOLE NO.: BH 3	
Project: 38-42 Gerathy Street, Goulburn				Date : April 8, 2024			
Location: Refer to Drawing No. 24/0904				Logged: MB      Checked By: MT		Sheet 1 of 1	
W A T T A E B R L E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  Soil Name, grain size /plasticity, colour; secondary constituents (Inc. Description) , minor constituents including other remarks		S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
	S2 @ 0.4 m	0.5	TOPSOIL: SILTY CLAY: low plasticity, brown		CL	—	>PL
			SILTY CLAY: low to medium plasticity, grey brown		CL/CI	FIRM STIFF	>PL
	U50	1.5	SILTY CLAY: medium plasticity, yellow brown, mottled grey, trace of gravel		CI	STIFF VERY STIFF	=PL
	2.0						
		2.5					
			BOREHOLE DISCONTINUED AT 3.0 M				
D - disturbed sample      U - undisturbed tube sample      B - bulk sample					Contractor: STS		
WT - level of water table or free water      N - Standard Penetration Test (SPT)					Equipment: Christie		
S - jar sample					Hole Diameter (mm): 100		
NOTES: See explanation sheets for meaning of all descriptive terms and symbols					Angle from Vertical (°): 0		
					Drill Bit: Spiral		



Client: Homes NSW Project: 38-42 Gerathy Street, Goulburn Location: Refer to Drawing No. 24/0904				Project: 32649/8602D-G Date : April 8, 2024 Logged: MB      Checked By: MT		BOREHOLE NO.: BH 5		
						Sheet 1 of 1		
W A T T A E B R L E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  Soil Name, grain size /plasticity, colour; secondary constituents (Inc. Description) , minor constituents including other remarks			S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
	S3 @ 0.7 m	0.5	TOPSOIL: SILTY CLAY: low plasticity, brown			CL	—	>PL
			SILTY CLAY: low plasticity, grey brown			CL	STIFF	>PL
	U50	1.5	SILTY CLAY: medium plasticity, yellow brown, mottled grey			CI	STIFF	=PL
	BOREHOLE DISCONTINUED AT 3.0 M				VERY STIFF			
D - disturbed sample      U - undisturbed tube sample      B - bulk sample WT - level of water table or free water      N - Standard Penetration Test (SPT) S - jar sample						Contractor: STS Equipment: Christie Hole Diameter (mm): 100		
NOTES: See explanation sheets for meaning of all descriptive terms and symbols						Angle from Vertical (°): 0 Drill Bit: Spiral		



## Dynamic Cone Penetrometer Test Report

Project: 38-42 GERATHY STREET, GOULBURN

Project No.: 32649/8602D

Client: HOMES NSW

Report No.: 24/0903

Address: 4 Parramatta Square, 12 Darcy Street, Parramatta

Report Date: April 15, 2024

Test Method: AS 1289.6.3.2

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Site No.	P1	P2	P3	P4	P5	
Location	Refer to Drawing No. 24/0904	Refer to Drawing No. 24/0904	Refer to Drawing No. 24/0904	Refer to Drawing No. 24/0904	Refer to Drawing No. 24/0904	
Date Tested	8/4/2024	8/4/2024	8/4/2024	8/4/2024	8/4/2024	
Starting Level	Surface Level	Surface Level	Surface Level	Surface Level	Surface Level	
Depth (m)	Penetration Resistance (blows / 150mm)					
0.00 - 0.15	2	2	2	2	2	
0.15 - 0.30	2	3	2	3	2	
0.30 - 0.45	2	2	4	3	3	
0.45 - 0.60	2	2	5	3	3	
0.60 - 0.75	3	4	5	4	5	
0.75 - 0.90	4	3	4	5	5	
0.90 - 1.05	4	4	8	7	4	
1.05 - 1.20	4	5	12	4	4	
1.20 - 1.35	4	16	16	4	6	
1.35 - 1.50	5	23+	23+	19	10	
1.50 - 1.65	4	Discontinued	Discontinued	23+	23+	
1.65 - 1.80	4			Discontinued	Discontinued	
1.80 - 1.95	6					
1.95 - 2.10	10					
2.10 - 2.25	12					
2.25 - 2.40	12					
2.40 - 2.55	23+					
2.55 - 2.70	Discontinued					
2.70 - 2.85						
2.85 - 3.00						
3.00 - 3.15						
3.15 - 3.30						
3.30 - 3.45						
3.45 - 3.60						
3.60 - 3.75						

Remarks: \* Pre drilled prior to testing

Approved Signatory.....



Technician: MB

Mrigesh Tamang

## EXPLANATION OF NOTES, ABBREVIATIONS & TERMS USED ON BOREHOLE AND TEST PIT LOGS

### DRILLING/EXCAVATION METHOD





<b>HA</b>	Hand Auger	<b>ADH</b>	Hollow Auger	<b>NQ</b>	Diamond Core - 47 mm
<b>DT</b>	Diatube Coring	<b>RT</b>	Rotary Tricone bit	<b>NMLC</b>	Diamond Core - 52 mm
<b>NDD</b>	Non-destructive digging	<b>RAB</b>	Rotary Air Blast	<b>HQ</b>	Diamond Core - 63 mm
<b>AD*</b>	Auger Drilling	<b>RC</b>	Reverse Circulation	<b>HMLC</b>	Diamond Core - 63 mm
<b>*V</b>	V-Bit	<b>PT</b>	Push Tube	<b>EX</b>	Tracked Hydraulic Excavator
<b>*T</b>	TC-Bit, e.g. AD/T	<b>WB</b>	Washbore	<b>HAND</b>	Excavated by Hand Methods

### PENETRATION RESISTANCE

<b>L</b>	<b>Low Resistance</b>	Rapid penetration/ excavation possible with little effort from equipment used.
<b>M</b>	<b>Medium Resistance</b>	Penetration/ excavation possible at an acceptable rate with moderate effort from equipment used.
<b>H</b>	<b>High Resistance</b>	Penetration/ excavation is possible but at a slow rate and requires significant effort from equipment used.
<b>R</b>	<b>Refusal/Practical Refusal</b>	No further progress possible without risk of damage or unacceptable wear to equipment used.

These assessments are subjective and are dependent on many factors, including equipment power and weight, condition of excavation or drilling tools and experience of the operator.

### WATER

	 <b>Standing Water Level</b>	 <b>Partial water loss</b>
	 <b>Water Seepage</b>	 <b>Complete Water Loss</b>
<b>GWNO</b>	GROUNDWATER NOT OBSERVED - Observation of groundwater, whether present or not, was not possible due to drilling water, surface seepage or cave-in of the borehole/ test pit.	
<b>GWNE</b>	GROUNDWATER NOT ENCOUNTERED - Borehole/ test pit was dry soon after excavation. However, groundwater could be present in less permeable strata. Inflow may have been observed had the borehole/ test pit been left open for a longer period.	

### SAMPLING AND TESTING

<b>SPT</b>	Standard Penetration Testing to AS1289.6.3.3 2004
4,7,11 N=18	4,7,11 = Blows per 150mm. N = Blows per 300mm penetration following a 150mm seating drive
30/80mm	Where practical refusal occurs, the blows and penetration for that interval are reported, N is not reported
RW	Penetration occurred under the rod weight only, N<1
HW	Penetration occurred under the hammer and rod weight only, N<1
HB	Hammer double bouncing on anvil, N is not reported
<b>Sampling</b>	
S1	Jar sample – number indicates sample number
D	Disturbed Sample
B	Bulk disturbed Sample
U50	Thin walled tube sample - number indicates nominal sample diameter in millimetres
<b>Testing</b>	
PP	Pocket Penetrometer test expressed as instrument reading in kPa
DCP	Dynamic Cone Penetrometer (AS1289.6.3.1 1997)
PSP	Perth Sand Penetrometer (AS1289.6.3.2 1997)

### GEOLOGICAL BOUNDARIES

————— = Observed Boundary (Position known)	- - - - - = Observed Boundary (Position approximate)	- -?- -?- -?- = Boundary (Interpreted or inferred)
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### ROCK CORE RECOVERY

TCR = Total Core Recovery (%)

$$= \frac{\text{Length of core recovered}}{\text{Length of core run}} \times 100$$

RQD = Rock Quality Designation (%)

$$= \frac{\sum \text{Axial lengths of core} > 100\text{mm}}{\text{Length of core run}} \times 100$$

## METHOD OF SOIL DESCRIPTION USED ON BOREHOLE AND TEST PIT LOGS



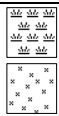
FILL



COUBLES or  
BOULDERS



GRAVEL (GP or GW)



ORGANIC SOILS  
(OL, OH or Pt)



SILT (ML or MH)

Combinations of these basic symbols may be used to indicate mixed materials such as sandy clay



CLAY (CL, CI or CH)



SAND (SP or SW)

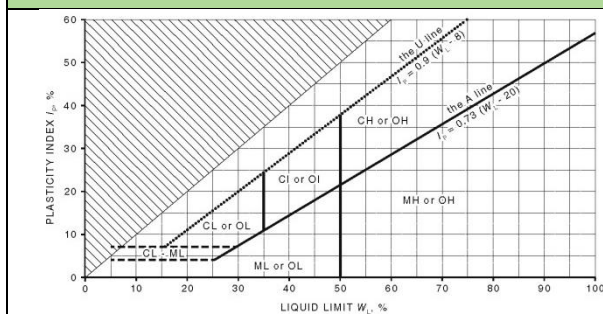
### CLASSIFICATION AND INFERRED STRATIGRAPHY

Soil is broadly classified and described in Borehole and Test Pit Logs using the preferred method given in AS 1726:2017, Section 6.1 – Soil description and classification.

#### PARTICLE SIZE CHARACTERISTICS

Fraction	Components	Sub Division	Size mm
Oversize	BOULDERS		>200
	COBBLES		63 to 200
Coarse grained soil	GRAVEL	Coarse	19 to 63
		Medium	6.7 to 19
		Fine	2.36 to 6.7
	SAND	Coarse	0.6 to 2.36
		Medium	0.21 to 0.6
		Fine	0.075 to 0.21
Fine grained soil	SILT		0.002 to 0.075
	CLAY		<0.002

#### PLASTICITY PROPERTIES



#### GROUP SYMBOLS

Major Divisions	Symbol	Description
COARSE GRAINED SOILS More than 65% of soil excluding oversize fraction is greater than 0.075mm	GRAVEL More than 50% of coarse fraction is >2.36mm	GW Well graded gravel and gravel-sand mixtures, little or no fines, no dry strength.
		GP Poorly graded gravel and gravel-sand mixtures, little or no fines, no dry strength.
		GM Silty gravel, gravel-sand-silt mixtures, zero to medium dry strength.
		GC Clayey gravel, gravel-sand-clay mixtures, medium to high dry strength.
	SAND More than 50% of coarse fraction is <2.36 mm	SW Well graded sand and gravelly sand, little or no fines, no dry strength.
		SP Poorly graded sand and gravelly sand, little or no fines, no dry strength.
		SM Silty sand, sand-silt mixtures, zero to medium dry strength.
		SC Clayey sand, sandy-clay mixtures, medium to high dry strength.
	FINE GRAINED SOILS More than 35% of soil excluding oversized fraction is less than 0.075mm	ML Inorganic silts of low plasticity, very fine sands, rock flour, silty or clayey fine sands, zero to medium dry strength.
		CL, CI Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, medium to high dry strength.
		OL Organic silts and organic silty clays of low plasticity, low to medium dry strength.
		MH Inorganic silts of high plasticity, high to very high dry strength.
Highly Organic soil	CH	Inorganic clays of high plasticity, high to very high dry strength.
	OH	Organic clays of medium to high plasticity, medium to high dry strength.
	PT	Peat muck and other highly organic soils.

#### MOISTURE CONDITION

Symbol	Term	Description
D	Dry	Non- cohesive and free running.
M	Moist	Soils feel cool, darkened in colour. Soil tends to stick together.
W	Wet	Soils feel cool, darkened in colour. Soil tends to stick together, free water forms when handling.

Moisture content of cohesive soils shall be described in relation to plastic limit (PL) or liquid limit (LL) for soils with higher moisture content as follows: Moist, dry of plastic limit ( $w < PL$ ); Moist, near plastic limit ( $w \approx PL$ ); Moist, wet of plastic limit ( $w > PL$ ); Wet, near liquid limit ( $w \approx LL$ ); Wet, wet of liquid limit ( $w > LL$ ).

#### CONSISTENCY

Symbol	Term	Undrained Shear Strength (kPa)	SPT "N" #
VS	Very Soft	$\leq 12$	$\leq 2$
S	Soft	$>12$ to $\leq 25$	$>2$ to $\leq 4$
F	Firm	$>25$ to $\leq 50$	$>4$ to $\leq 8$
St	Stiff	$>50$ to $\leq 100$	$>8$ to $\leq 15$
VSt	Very Stiff	$>100$ to $\leq 200$	$>15$ to $\leq 30$
H	Hard	$>200$	$>30$
Fr	Friable	-	-

#### DENSITY

Symbol	Term	Density Index %	SPT "N" #
VL	Very Loose	$\leq 15$	0 to 4
L	Loose	$>15$ to $\leq 35$	4 to 10
MD	Medium Dense	$>35$ to $\leq 65$	10 to 30
D	Dense	$>65$ to $\leq 85$	30 to 50
VD	Very Dense	$>85$	Above 50

In the absence of test results, consistency and density may be assessed from correlations with the observed behaviour of the material.

# SPT correlations are not stated in AS1726:2017, and may be subject to corrections for overburden pressure, moisture content of the soil, and equipment type.

#### MINOR COMPONENTS

Term	Assessment Guide	Proportion by Mass
Add 'Trace'	Presence just detectable by feel or eye but soil properties little or no different to general properties of primary component	Coarse grained soils: $\leq 5\%$ Fine grained soil: $\leq 15\%$
Add 'With'	Presence easily detectable by feel or eye but soil properties little or no different to general properties of primary component	Coarse grained soils: 5 - 12% Fine grained soil: 15 - 30%
Prefix soil name	Presence easily detectable by feel or eye in conjunction with the general properties of primary component	Coarse grained soils: $>12\%$ Fine grained soil: $>30\%$

## CLASSIFICATION AND INFERRED STRATIGRAPHY

Rock is broadly classified and described in Borehole and Test Pit Logs using the preferred method given in AS1726 – 2017, Section 6.2 – Rock identification, description and classification.

## ROCK MATERIAL STRENGTH CLASSIFICATION

Symbol	Term	Point Load Index, $Is_{(50)}$ (MPa) #	Field Guide
VL	Very Low	0.03 to 0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxial sample by hand. Pieces up to 30 mm can be broken by finger pressure.
L	Low	0.1 to 0.3	Easily scored with a knife; indentations 1 mm to 3 mm show in the specimen with firm blows of pick point; has dull sound under hammer. A piece of core 150 mm long by 50 mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.
M	Medium	0.3 to 1	Readily scored with a knife; a piece of core 150 mm long by 50 mm diameter can be broken by hand with difficulty.
H	High	1 to 3	A piece of core 150 mm long by 50 mm diameter cannot be broken by hand but can be broken with pick with a single firm blow; rock rings under hammer.
VH	Very High	3 to 10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.
EH	Extremely High	>10	Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.

### # Rock Strength Test Results



Point Load Strength Index,  $Is_{(50)}$ , Axial test (MPa)



Point Load Strength Index,  $Is_{(50)}$ , Diametral test (MPa)

Relationship between rock strength test result ( $Is_{(50)}$ ) and unconfined compressive strength (UCS) will vary with rock type and strength, and should be determined on a site-specific basis. However UCS is typically  $20 \times Is_{(50)}$ .

## ROCK MATERIAL WEATHERING CLASSIFICATION

Symbol	Term	Field Guide
RS	Residual Soil	Soil developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported.
XW	Extremely Weathered	Rock is weathered to such an extent that it has soil properties - i.e. it either disintegrates or can be remoulded, in water.
DW	HW	Rock strength usually changed by weathering. The rock may be highly discoloured, usually by iron staining. Porosity may be increased by leaching, or may be decreased due to deposition of weathering products in pores. In some environments it is convenient to subdivide into Highly Weathered and Moderately Weathered, with the degree of alteration typically less for MW.
	MW	
SW	Slightly Weathered	Rock slightly discoloured but shows little or no change of strength relative to fresh rock.
FR	Fresh	Rock shows no sign of decomposition or staining.

## ABBREVIATIONS AND DESCRIPTIONS FOR ROCK MATERIAL AND DEFECTS

### CLASSIFICATION AND INFERRED STRATIGRAPHY

Rock is broadly classified and described in Borehole and Test Pit Logs using the preferred method given in AS1726 – 2017, Section 6.2 – Rock identification, description and classification.

### DETAILED ROCK DEFECT SPACING

Defect Spacing			Bedding Thickness (Stratification)	
Spacing/width (mm)	Descriptor	Symbol	Term	Spacing (mm)
<20	Extremely Close	EC	Thinly laminated	<6
20-60	Very Close	VC	Laminated	6 – 20
60-200	Close	C	Very thinly bedded	20 – 60
200-600	Medium	M	Thinly bedded	60 – 200
600-2000	Wide	W	Medium bedded	200 – 600
2000-6000	Very Wide	VW	Thickly bedded	600 – 2,000
			Very thickly bedded	> 2,000

### ABBREVIATIONS AND DESCRIPTIONS FOR DEFECT TYPES

Defect Type	Abbr.	Description
Joint	JT	Surface of a fracture or parting, formed without displacement, across which the rock has little or no tensile strength. May be closed or filled by air, water or soil or rock substance, which acts as cement.
Bedding Parting	BP	Surface of fracture or parting, across which the rock has little or no tensile strength, parallel or sub-parallel to layering/ bedding. Bedding refers to the layering or stratification of a rock, indicating orientation during deposition, resulting in planar anisotropy in the rock material.
Contact	CO	The surface between two types or ages of rock.
Sheared Surface	SSU	A near planar, curved or undulating surface which is usually smooth, polished or slickensided.
Sheared Seam/ Zone (Fault)	SS/SZ	Seam or zone with roughly parallel almost planar boundaries of rock substance cut by closely spaced (often <50 mm) parallel and usually smooth or slickensided joints or cleavage planes.
Crushed Seam/ Zone (Fault)	CS/CZ	Seam or zone composed of disoriented usually angular fragments of the host rock substance, with roughly parallel near-planar boundaries. The brecciated fragments may be of clay, silt, sand or gravel sizes or mixtures of these.
Extremely Weathered Seam/ Zone	XWS/XWZ	Seam of soil substance, often with gradational boundaries, formed by weathering of the rock material in places.
Infilled Seam	IS	Seam of soil substance, usually clay or clayey, with very distinct roughly parallel boundaries, formed by soil migrating into joint or open cavity.
Vein	VN	Distinct sheet-like body of minerals crystallised within rock through typically open-space filling or crack-seal growth.

NOTE: Defects size of <100mm SS, CS and XWS. Defects size of >100mm SZ, CZ and XWZ.

### ABBREVIATIONS AND DESCRIPTIONS FOR DEFECT SHAPE AND ROUGHNESS

Shape	Abbr.	Description	Roughness	Abbr.	Description
Planar	PR	Consistent orientation	Polished	POL	Shiny smooth surface
Curved	CU	Gradual change in orientation	Slickensided	SL	Grooved or striated surface, usually polished
Undulating	UN	Wavy surface	Smooth	SM	Smooth to touch. Few or no surface irregularities
Stepped	ST	One or more well defined steps	Rough	RO	Many small surface irregularities (amplitude generally <1mm). Feels like fine to coarse sandpaper
Irregular	IR	Many sharp changes in orientation	Very Rough	VR	Many large surface irregularities, amplitude generally >1mm. Feels like very coarse sandpaper

#### Orientation:

**Vertical Boreholes** – The dip (inclination from horizontal) of the defect.

**Inclined Boreholes** – The inclination is measured as the acute angle to the core axis.

### ABBREVIATIONS AND DESCRIPTIONS FOR DEFECT COATING

Coating	Abbr.	Description	Aperture	Abbr.	Description
Clean	CN	No visible coating or infilling	Closed	CL	Closed.
Stain	SN	No visible coating but surfaces are discoloured by staining, often limonite (orange-brown)	Open	OP	Without any infill material.
Veneer	VNR	A visible coating of soil or mineral substance, usually too thin to measure (< 1 mm); may be patchy	Infilled	-	Soil or rock i.e. clay, silt, talc, pyrite, quartz, etc.

## APPENDIX B – LABORATORY TEST RESULTS

## Shrink Swell Index Report

Project: 38 - 42 Gerathy Street, Gouburn

Client: Homes NSW

Address: 4 Parramatta Square, Darcy Street, Parramatta

Test Method: AS1289.7.1.1

Project No.: 32649

Report No.: 24/0908

Report Date: 16/04/2024

Page: 1 of 1

Sampling Procedure: AS 1289.1.3.1 Clause 3.1.3.2 - Thin Walled Sampler

STS / Sample No.		8602D-L/1	8602D-L/2	8602D-L/3			
Sample Location		Borehole 1 Refer to Drawing No. 24/0904	Borehole 3 Refer to Drawing No. 24/0904	Borehole 5 Refer to Drawing No. 24/0904			
Material Description		Silty Clay, yellow brown with Gravel	Silty Clay, yellow brown with Sand	Silty Clay, yellow brown orange with Sand			
Depth (m)		0.8 - 1.0	1.2 - 1.4	1.0 - 1.2			
Sample Date		8/04/2024	8/04/2024	8/04/2024			
Shrink	Moisture Content (%)	26.3	21.8	19.9			
	Soil Crumbling	Nil	Nil	Nil			
	Extent of Cracking	Fine Cracks	Fine Cracks	Fine Cracks			
	Strain (%)	4.9	3.5	1.6			
Swell	Moisture Content Initial (%)	19.5	22.9	19.0			
	Moisture Content Final (%)	27.3	26.0	20.4			
	Strain (%)	0.0	1.1	0.0			
Inert Inclusions (%)		<25	<10	<25			
Shrink Swell Index (%)		2.7	2.2	0.9			

Remarks:

Approved Signatory.....



Technician: DH

David Ly - Senior Geotechnician





## CERTIFICATE OF ANALYSIS

Work Order	: ES2411418	Page	: 1 of 2
Client	: STS Geotechnics	Laboratory	: Environmental Division Sydney
Contact	: ENQUIRES STS	Contact	: Customer Services ES
Address	: Unit 14/1 Cowpasture Place Wetherill Park 2164	Address	: 277-289 Woodpark Road Smithfield NSW Australia 2164
Telephone	: ----	Telephone	: +61-2-8784 8555
Project	: 30060/32649	Date Samples Received	: 09-Apr-2024 12:20
Order number	: 2024-126	Date Analysis Commenced	: 11-Apr-2024
C-O-C number	: ----	Issue Date	: 16-Apr-2024 12:08
Sampler	: IS, MB		
Site	: ----		
Quote number	: EN/222		
No. of samples received	: 4		
No. of samples analysed	: 4		



Accreditation No. 825  
Accredited for compliance with  
ISO/IEC 17025 - Testing

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with Quality Review and Sample Receipt Notification.

### Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories	Position	Accreditation Category
Ankit Joshi	Senior Chemist - Inorganics	Sydney Inorganics, Smithfield, NSW



## General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contract for details.

Key : CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.  
 LOR = Limit of reporting  
 ^ = This result is computed from individual analyte detections at or above the level of reporting  
 ø = ALS is not NATA accredited for these tests.  
 ~ = Indicates an estimated value.

- ED045G: LOR raised for Chloride due to sample matrix.
- ED045G: The presence of Thiocyanate, Thiosulfate and Sulfite can positively contribute to the chloride result, thereby may bias results higher than expected. Results should be scrutinised accordingly.

## Analytical Results

Sub-Matrix: SOIL  
 (Matrix: SOIL)

Sample ID

				30060/1903	32649/S1	32649/S2	32649/S3	----
Sampling date / time				08-Apr-2024 00:00	08-Apr-2024 00:00	08-Apr-2024 00:00	08-Apr-2024 00:00	----
Compound	CAS Number	LOR	Unit	ES2411418-001	ES2411418-002	ES2411418-003	ES2411418-004	-----
Result				Result	Result	Result	Result	----
<b>EA002: pH 1:5 (Soils)</b>								
pH Value	----	0.1	pH Unit	5.6	7.7	7.9	8.0	----
<b>EA010: Conductivity (1:5)</b>								
Electrical Conductivity @ 25°C	----	1	µS/cm	42	70	38	46	----
<b>EA055: Moisture Content (Dried @ 105-110°C)</b>								
Moisture Content	----	0.1	%	16.6	15.7	15.4	13.9	----
<b>ED040S : Soluble Sulfate by ICPAES</b>								
Sulfate as SO4 2-	14808-79-8	10	mg/kg	<10	<10	<10	10	----
<b>ED045G: Chloride by Discrete Analyser</b>								
Chloride	16887-00-6	10	mg/kg	----	20	<50	<50	----